## Appendix A Hydrologic Data for Maine

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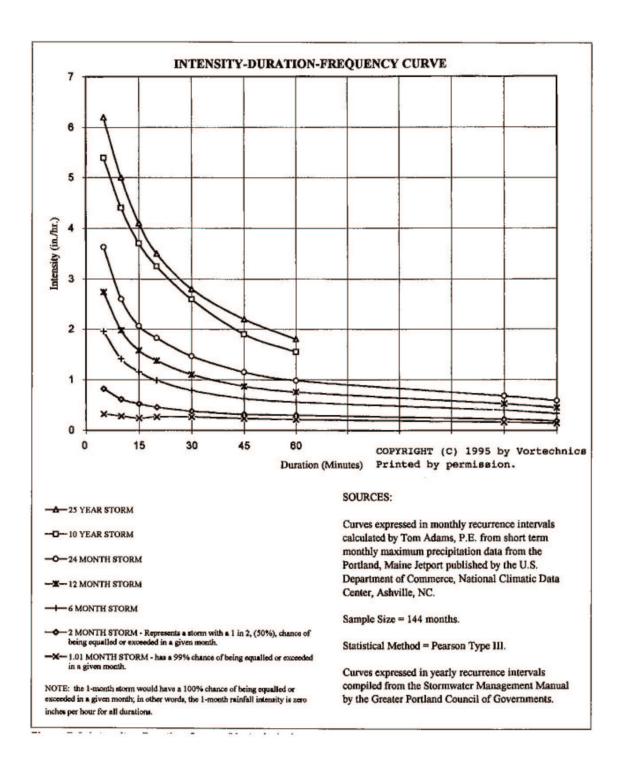
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#### **Appendix A-1: Intensity-Duration Curves (Vortechnics)**



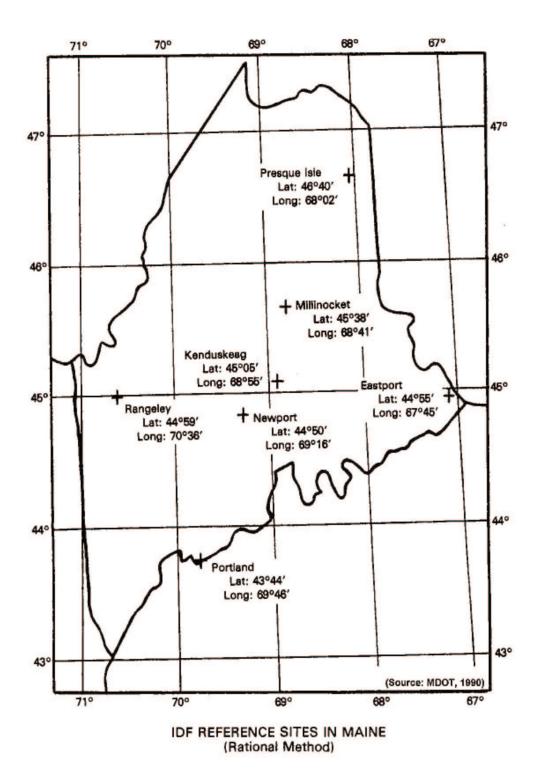
#### **Appendix A-2: Portland & Cumberland County Precipitation Intensity/Duration (COG)**

						Portland &	Cumbert	and County					
		Precipitation Intensity/Duration											
		Cumb. Co. (NOAA 35)	Portland (COG '81	5 ye Cumb. Co. 7 (NOAA 35)	ears Portland (COG '81		ears Portland (COG '81	25 yea Cumb. Co. ) (NOAA 35)	Portland	Cumb. C	0 years 0. Port 5)(COG		100 years Co. Portland
5	minute	0.34	0.312	0.40	0.368	0.45	0.410	0,52	0.471	0.58	0.520	0.63	0.568
10	minute	0.51	0.480	0.63	0.573	0.72	0.641	0.84	0.739	0.93	0.818	1.03	0.895
15	minute	0.63	0.579	0.79	0.699	0.90	0.786	1.05	0.912	1.18	1.01	1.30	1.11
30	minute	0.83	0.758	1.07	0.948	1.23	1.08	1.46	1.27	1.64	1.42	1.82	1.57
1	hour	1.04 (TP 40)	1.00	1.36 (TP 40)	1.24	1.58 (TP 40)	1.40	1.89 (TP 40)	1.65	2.13 (TP 40)	1.83	2.37 (TP 40)	2.02
2	hours	(TP 40)	1.30	(TP 40)	1.46	(TP 40)	1.59	(TP 40) 2.45	1.78	(TP 40)	1.94	(TP 40)	2.09
3	hours	1.6		2,1		2.45		2.7		3,1		3.5	
6	hours	2.1		2.65		3.1		3.4		4.0		4.4	
12	hours	2.5		3.4		3.9		4.8		5.0		5.7	
24	hours	3.0	3.18	4.0	3.87	4.7	4.37	5.5	5.08	5.8	5.65	6.7	6.21

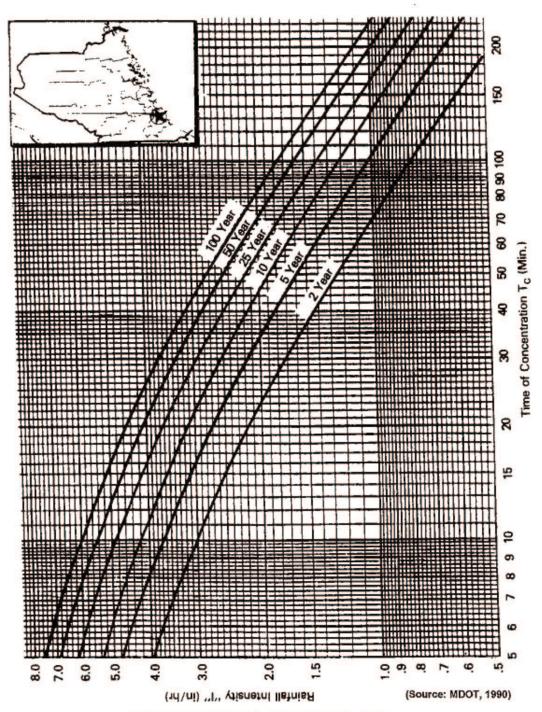
TP 40 = "Rainfall Frequency Atlas", Government Printing Office, 1961
NOAA 35 = "Five to 60 Minute Precipitation Frequency for the Eastern and Central U.S.", National Weather Service
1977.
COG '81 = Hand calculations by Joan Feely (GPCOG intern), from "Rainfall Intensity-Frequency Analysis"
- Form 612-47, Environmental Science Services Admin., Weather Bureau, adjusted for partial-duration series as in NOAA 35.

(Source: GPCOG, 1981)

#### **Appendix A-3: IDF Reference Sites in Maine (MDOT)**



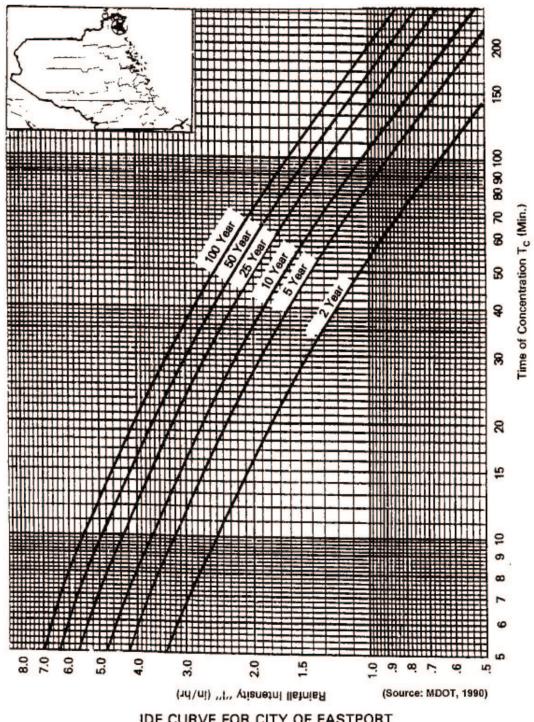
### **Appendix A-4: IDF Curve for City of Portland**



IDF CURVE FOR CITY OF PORTLAND
(Rational Method)

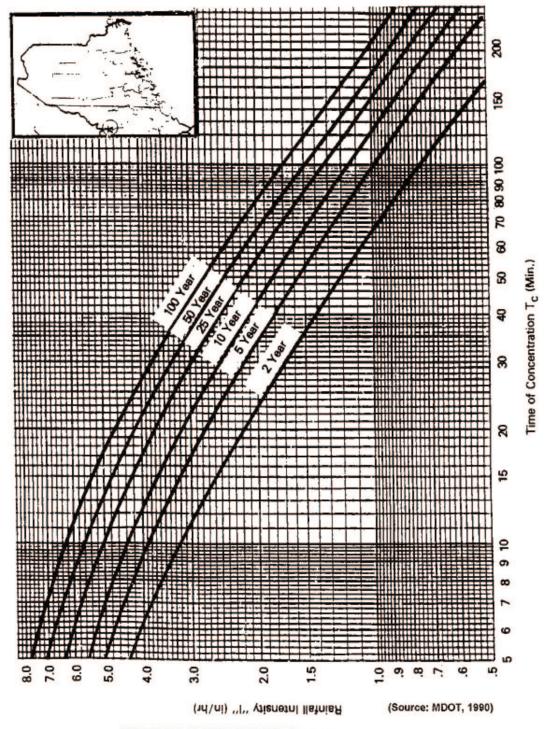
3

### **Appendix A-5: IDF Curve for City of Eastport**



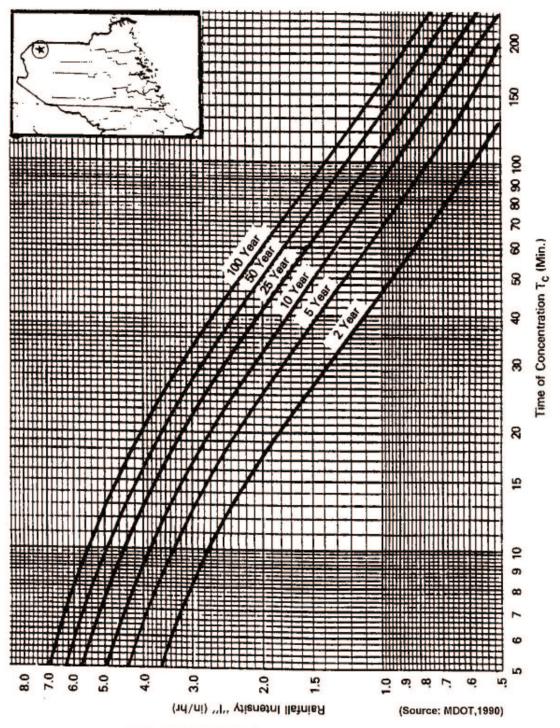
IDF CURVE FOR CITY OF EASTPORT (Rational Method)

### **Appendix A-6: IDF Curve for Town of Rangeley**



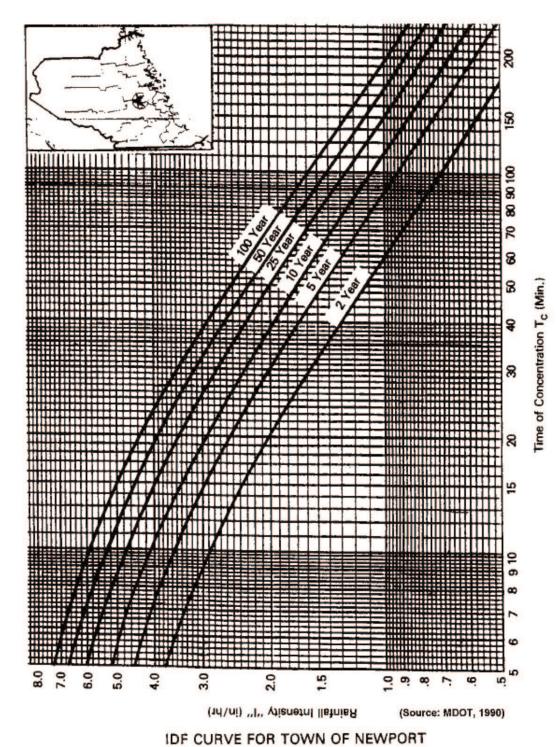
IDF CURVE FOR TOWN OF RANGELEY (Rational Method)

### **Appendix A-7: IDF Curve for City of Presque Isle**



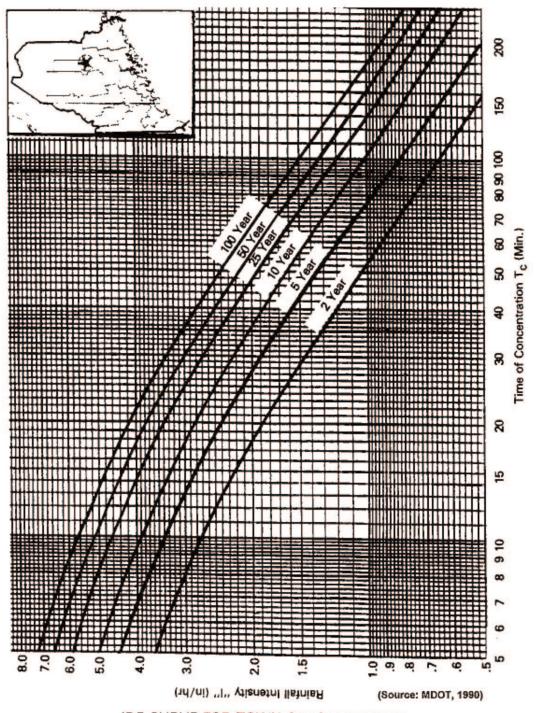
IDF CURVE FOR CITY OF PRESQUE ISLE (Rational Method)

#### **Appendix A-8: IDF Curve for Town of Newport**



(Rational Method)

#### **Appendix A-9: IDF Curve for Town of Millinocket**



IDF CURVE FOR TOWN OF MILLINOCKET (Rational Method)

#### **Appendix A-10: Runoff Coefficients for the Rational Formula**

Typical Composite Runot Land Use.	ff Coefficients by	Normal Range of Runoff Coefficients.					
Description of Area	C-value	Character of Surface	C-value				
Business:		Lawns:					
Downtown areas	0.70-0.95	Sandy soil, flat (2%)	0.05-0.10				
Neighborhood areas	0.50-0.70	Sandy soil, ave. (2-7%)	0.10-0.15				
25 Aug 2004		Sandy soil, steep (7%)	0.15-0.20				
Residential:		Heavy soil, flat (2%)	0.13-0.17				
Single-family areas	0.30-0.50	Heavy soil, ave. (2-7%)	0.18-0.22				
Multi units, detached	0.40-0.60	Heavy soil, steep (7%)	0.25-0.35				
Multi units, attached	0.60-0.75	Agricultural land:					
Suburban	0.25-0.40	Bare packed soil					
Apartment	0.50-0.70	Smooth	0.30-0.60				
Industrial:	10321 3203972	Rough	0.20-0.50				
Light areas	0.50-0.80	Cultivated rows	Contract to the state of				
Heavy areas	0.60-0.90	Heavy soils, no crop	0.30-0.60				
	18 (2004) 25550013	Heavy soils with crop	0.20-0.50				
Parks, cemeteries	0.10-0.25	Sandy soil no crop	0.20-0.40				
	Antest La Shapers	Sandy soil with crop	0.10-0.25				
Playgrounds	0.20-0.35	Pasture	1000 0000000000000000000000000000000000				
		Heavy soil	0.15-0.45				
Railroad yard areas	0.20-0.35	Sandy soil	0.05-0.25				
		Woodlands	0.05-0.25				
Unimproved areas	0.10-0.30	Pavement					
_		Asphalt and Concrete	0.70-0.95				
		Brick	0.70-0.85				
		Roofs	0.75-0.95				

NOTE: The designer must use judgment to select the appropriate "C" value within the range for the appropriate land use. Generally, larger areas with permeable soils, flat slopes, and dense vegetation should have lowest "C" values. Smaller areas with slowly permeable soils, steep slopes, and sparse vegetation should be assigned highest "C" values. The range of "C" values presented are typical for return periods of 2-10 years. Higher values are appropriate for larger design storms. (ASCE 1992 and others)

Appendix A-11: Runoff Coefficients for the Rational Formula by Hydrologic Soil Group and Slope

	٨			В			C			D		
Land use	0-2%	2-6%	6%+	0-2%	2-6%	6%+	0-2%	2-6%	6%+	0-2%	2-6%	6%+
Cultivated land	0.08	0.13	0.16 0.22	0.11 0.16	0.15	0.21 0.28	0.14	0.19	0.26	0.18 0.24	0.23	0.31
Pasture	0.12 0.15	0.20 0.25	0.30	0.18	0.28 0.34	0.37	0.24	0.34	0.44	0.30 0.37	0.40	0.50
Meadow	0.10 0.14	0.16 0.22	0.25	0.14	0.22 0.28	0.30 0.37	0.20 0.26	0.28	0.36 0.44	0.24	0.30	0.40
Forest	0.05	0.08	0.11	80.0	0.11	0.14	0.10	0.13	0.16	0.12 0.15	0.16 0.20	0.20
Residential Lot size acre (0.05 ha)	0.25 0.33	0.28 0.37	0.31	0.27 0.35	0.30 0.39	0.35	0.30 0.38	0.33	0.38	0.33 0.41	0.36 0.45	0.42
(0.10 ha)	0.22	0.26	0.29	0.24	0.29	0.33	0.27 0.36	0.31	0.36	0.30	0.34	0.40
Lot size ; acre (0.13 ha)	0.19	0.23	0.26 0.35	0.22	0.26	0.30	0.25	0.29	0.45	0.28	0.32	0.39
Lot size 3 acre (0.2 ha)	0.16	0.20	0.24	0.19	0.23	0.28	0.22	0.27	0.32	0.26	0.30	0.37
Lot size 1 acre (0.4 ha)	0.14 0.22	0.19 0.26	0.22	0.17	0.21	0.26	0.20	0.25	0.31	0.24	0.29	0.35
Industrial	0.67	0.68	0.68	0.68	0.68	0.69	0.68	0.69	0.69	0.69	0.69	0.70
Commercial	0.71	0.71	0.72 0.89	0.71	0.72	0.72	0.72	0.72	0.72	0.72	0.72	0.72
Streets	0.70 0.76	0.71 0.77	0.72	0.71	0.72 0.82	0.74	0.72	0.73	0.76	0.73	0.75 19.0	0.78
Open space	0.05	0.10	0.14	0.08	0.13	0.19	0.12	0.17	0.24	0.16	0.21	0.28
Parking	0.85	0.86 0.96	0.87	0.85	0.86 0.96	0.87	0.85	0.86	0.87	0.85	0.86	0.87

(Source: Rawls et al., 1981, and Browne, 1990)

#### Appendix A-12: Runoff Curve Numbers for use in TR-55 and **TR-20**

	Hydrologic Soil Group					
Land Use/Cover type and hydrologic condition	A	В	C	D		
Cultivated Land						
without conservation	72	81	88	91		
with conservation	62	71	78	81		
Will Colloc Fation	02	7.1	70	01		
Pasture land						
poor condition: heavily grazed, no mulch	68	79	86	89		
fair condition: 50 to 75% ground cover	49	69	79	84		
good condition: lightly grazed, > 75% ground cover	39	61	74	80		
Meadow (protected from grazing)	30	58	71	78		
Wood or forest land						
Thin stand - poor cover, no mulch, burned over	45	66	77	83		
Good stand - good cover, litter and brush cover soil	25	55	70	77		
Sood stated good cover, into the state cover son	25	23	10	11		
Wood yard (log storage)	72	82	87	89		
Open space, lawns, parks, golf courses, cemeteries, etc.						
Good condition: grass cover on 75% or more of the area	39	61	74	80		
Fair condition: grass cover on 50 to 75 % of the area	49	69	79	84		
Commercial and business areas (85% impervious)	89	92	94	95		
Industrial districts (72% impervious)	81	88	91	93		
Residential: Development completed, vegetation established, house						
and driveway drains toward road						
Average lot size Average % impervious						
1/8 acre or less (town houses) 65	77	85	90	92		
1/4 acre 38	61	75	83	87		
1/3 acre 30	57	72	81	86		
1/2 acre 25	54	70	80	85		
1 acre 20	51	68	79	84		
2 acre 15	46	65	77	82		
Paved parking lots, roofs, driveways, etc.(excluding R-O-W)	98	98	98	98		
Streets and roads						
Paved with curb and storm sewers (excluding R-O-W)	98	98	98	98		
Paved with ditches (including R-O-W)	83	89	92	93		
Gravel (including R-O-W)	76	85	89	91		
Dirt (including R-O-W)	72	82	87	89		
Zar (anothering re-o-re)	12	02	01	09		
Newly graded area (denuded)	77	86	91	94		

Note: Average runoff condition and  $I_a = 0.2S$ Source: SCS, 1986 and DEP staff.

# **Appendix A-13: Curve Number Adjustments Based on Differing AMCs**

CN for	CN for	CN for	S* value		ostants for the CN for	CN for	CN for	S* value	
AMC II	AMC I	AMC III	(in.)	Ia	AMC II	AMC I	AMC III	(in.)	Ia
100	100	100	0	0	60	40	78	6.67	1.33
99	97	100	0.101	0.02	59	39	77	6.95	1.39
98	94	99	0.204	0.04	58	38	76	7.24	1.45
97	91	99	0.309	0.06	57	37	75	7.54	1.51
96	89	99	0.417	0.08	56	36	75	7.86	1.57
95	87	98	0.526	0.11	55	35	74	8.18	1.64
94	85	98	0.638	0.13	54	34	73	8.52	1.70
93	83	98	0.753	.015	53	33	72	8.87	1.77
92	81	97	0.870	.017	52	32	71	9.23	1.85
91	80	97	0.989	0.20	51	31	70	9.61	1.92
90	78	96	1.11	0.22	50	31	70	10.0	2.00
89	76	96	1.24	0.25	49	30	69	10.4	2.08
88	75	95	1.36	0.27	48	29	68	10.8	2.16
87	73	95	1.49	0.30	47	28	67	11.3	2.26
86	72	94	1.63	0.33	46	27	66	11.7	2.34
85	70	94	1.76	0.35	45	26	65	12.2	2.44
84	68	93	1.90	0.38	44	25	64	12.7	2.54
83	67	93	2.05	0.41	43	25	63	13.2	2.64
82	66	92	2.20	0.44	42	24	62	13.8	2.76
81	64	92	2.34	0.47	41	23	61	14.4	2.88
80	63	91	2.50	0.50	40	22	60	15.0	3.00
79	62	91	2.66	0.53	39	21	59	15.6	3.12
78	60	90	2.82	0.56	38	21	58	16.3	3.26
77	59	89	2.99	0.60	37	20	57	17.0	3.40
76	58	89	3.16	0.63	36	19	56	17.8	3.56
75	57	88	3.33	0.67	35	18	55	18.6	3.72
74	55	88	3.51	0.70	34	18	54	19.4	3.88
73	54	87	3.70	0.74	33	17	53	20.3	4.06
72	53	86	3.89	0.78	32	16	52	21.2	4.24
71	52	86	4.08	0.82	31	16	51	22.2	4.44
70	51	85	4.28	0.86	30	15	50	23.3	4.66
69	50	84	4.49	0.90					
68	48	84	4.70	0.94	25	12	43	30.0	6.00
67	47	83	4.92	0.98	20	9	37	40.0	8.00
66	46	82	5.15	1.03	15	6	30	56.7	11.34
65	45	82	5.38	1.08	10	4	22	90.0	18.00
64	44	81	5.62	1.12	5	2	13	190.0	38.00
63	43	80	5.87	1.17	0	0	0	00	00
62	42	79	6.13	1.23	X300	350	188	C. C. C. C.	
61	41	78	6.39	1.28					

Source: Browne, 1990; SCS 1972

<sup>\*</sup>For CN listed for AMC Condition II; S=((1000/CN)-10),  $I_a$ =0.2S